M/C DESIGN

- Length of open belt drive (O.B.D
$$= 2C + \frac{\pi}{2}(D_1 + D_2) + \frac{(D_2 - D_1)^2}{4C}$$
- Length of cross belt driven (C.B.D)
$$= 2C + \frac{\pi}{2}(D_1 + D_2) + \frac{(D_2 + D_1)^2}{4C}$$
- Velocity ratio
$$V.R = \frac{N_2}{N_1} = \left(\frac{D_1 + t}{D_2 + t}\right)\left(1 - \frac{S}{100}\right)$$
- Ratio of belt tension $\frac{T_1}{T_2} = e^{\mu\theta}$
- Maximum tensile strength of belt
$$T_{max} = b.t.\sigma_{per}$$
- Power transmission capacity of belt drive
$$P.T.C = (T_1 - T_2)v$$
- Centrifugal tension $T_c = \frac{T_{max}}{3}$
- Initial tension $T_0 = \frac{T_1 + T_2 + 2T_c}{2}$
- Number of 'V' belts $n = \frac{P_{total}}{P_{each}} \times K_a$
- Buckingham dynamic load
$$F_d = F_t + \frac{20.67v(bc + F_t)}{20.67v + \sqrt{bc + F_t}}$$
$$c = \frac{e}{K\left(\frac{1}{E_1} + \frac{1}{E_2}\right)}$$
- Soderberg equation $\frac{1}{FOS} = \frac{\sigma_m}{\sigma_{yt}} + \frac{K_f\sigma_v}{\sigma_e}$
- Goodman equation $\frac{1}{FOS} = \frac{K_f\sigma_m}{\sigma_{ut}} + \frac{K_f\sigma_v}{\sigma_e}$
- Notch sensitivity index $q = \frac{K_f - 1}{K_t - 1}$
- Unwin's formula $d = 6\sqrt{t}$

- Area of transverse fillet weld
$$A_{T.F.W} = h\ell_e, \quad h = \frac{t}{\cos\theta + \sin\theta}$$
- Strength of T.F.W $= 0.832t\ell_e\tau_{per}$
- Strength of parallel fillet weld
$= 0.707t\ell_e\tau_{per}$
- Strength of Butt weld $= h\ell(\sigma_t)_{per}$
- Frictional torque of thrust bearing by uniform pressure theory
$$(T_f)_{UPT} = \frac{2}{3}\mu\omega\left(\frac{R_o^3 - R_i^3}{R_o^2 - R_i^2}\right)$$
- Frictional torque of thrust bearing by uniform wear theory
$$(T_f)_{UWT} = \mu\omega\left(\frac{R_o + R_i}{2}\right)$$
- Power less $P_{loss} = T_f.\omega$
- T_f equations for flat pivot bearing
$$(T_f)_{UPT} = \frac{2}{3}\mu WR \qquad (T_f)_{UWT} = \frac{1}{2}\mu WR$$
- Bearing pressure $p_{ind} = \frac{W}{L.D}$
- Strength of bearing $= p_{per} \times L \times D$
- Bearing characteristic number $= \frac{zn}{p}$
- Mc-Kee's equation
$$\mu = \frac{33}{10^8}\left[\left(\frac{zn'}{p'}\right)\left(\frac{D}{C}\right)\right] + K$$
- Somer field No. $S = \left(\frac{zn}{p}\right)\left(\frac{D}{C}\right)^2$ (n in rps)
- Petroff's equation for μ $\mu = 2\pi^2\left(\frac{zn}{p}\right)\left(\frac{D}{C}\right)$
- Life of bearing $L_{90} = \left(\frac{C}{P_e}\right)^k$ (Million rev.)

K_a = Service or overload factor.

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Thirumalaisamy P. Velavancorresponding

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